

Prepared for:

NEW CENTRE WILMINGTON, LLC

806 GREEN VALLEY ROAD, SUITE 311
GREENSBORO, NC 27408

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PLANNING DIVISION

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Stormwater & Erosion Control Calculations

New Centre Apartments Fitness

Center

New Hanover County, NC
City of Wilmington

May 25, 2016

Revised July 29, 2016

Revised October 28, 2016

Final Calcs
12/1/16
DP2016044
rac

Curry
ENGINEERING

Prepared by:

Zak Shipman, P.E.
The Curry Engineering Group, PLLC
PO Box 2018
205 S. Fuquay Ave.
Fuquay-Varina, NC 27526
(919)552-0849

NORTH CAROLINA
PROFESSIONAL
ENGINEER
WILLIAM Z. SHIPMAN
035027
11-24-16

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NOV 09 2016

ENGINEERING

TABLE OF CONTENTS

SUPPORT DOCUMENTS

USGS Topography Map
FEMA Floodplain Maps
NRCS Soils Information
NOAA Precipitation Data

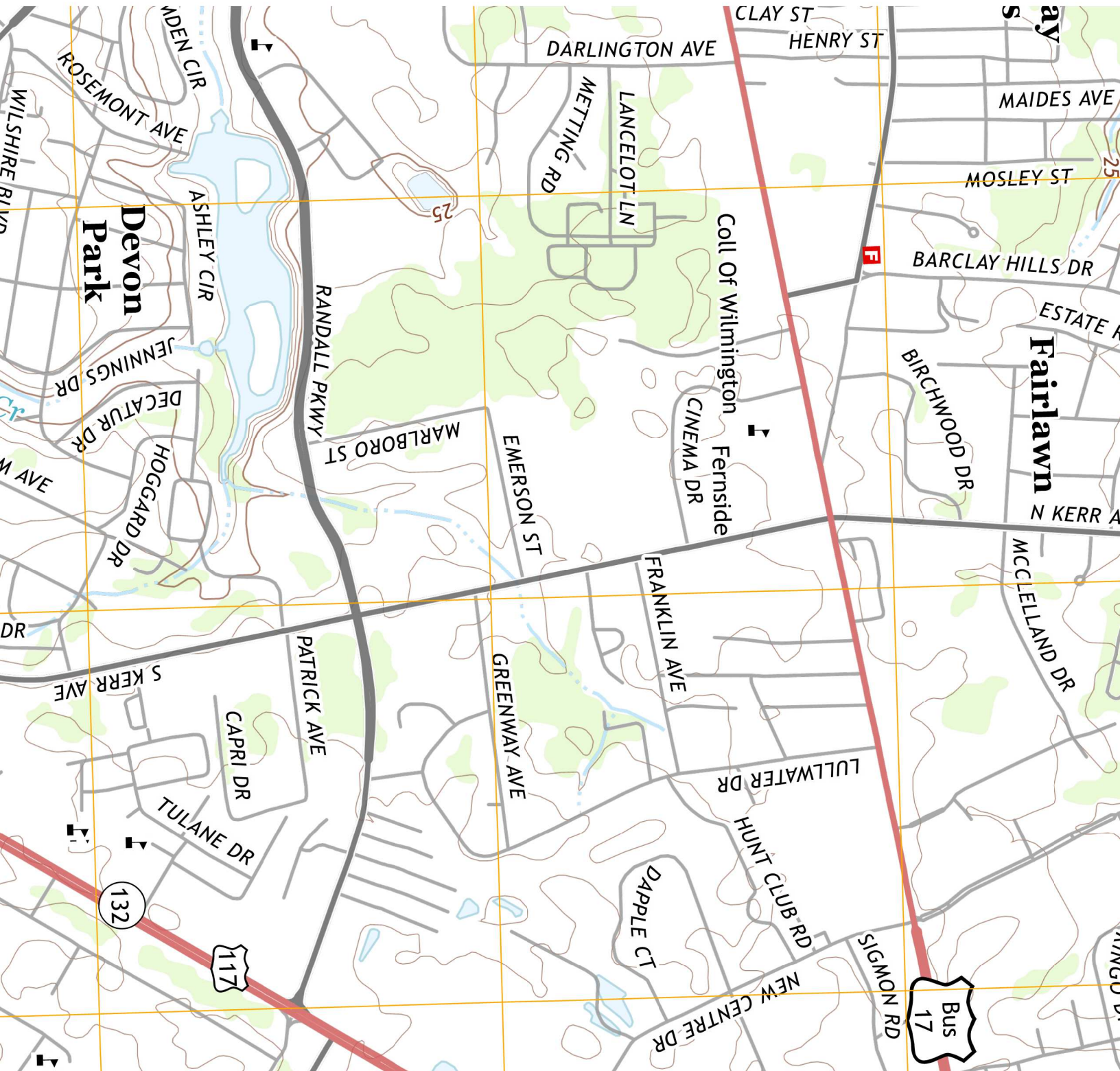
CALCULATIONS & ANALYSIS

Stormwater-Storm Sewer Pipe Network Calculations
Stormwater BMP Calculations

T (919) 552-0849
F (919) 552-2043

205 S. Fuquay Avenue
Fuquay-Varina, NC 27526





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3792

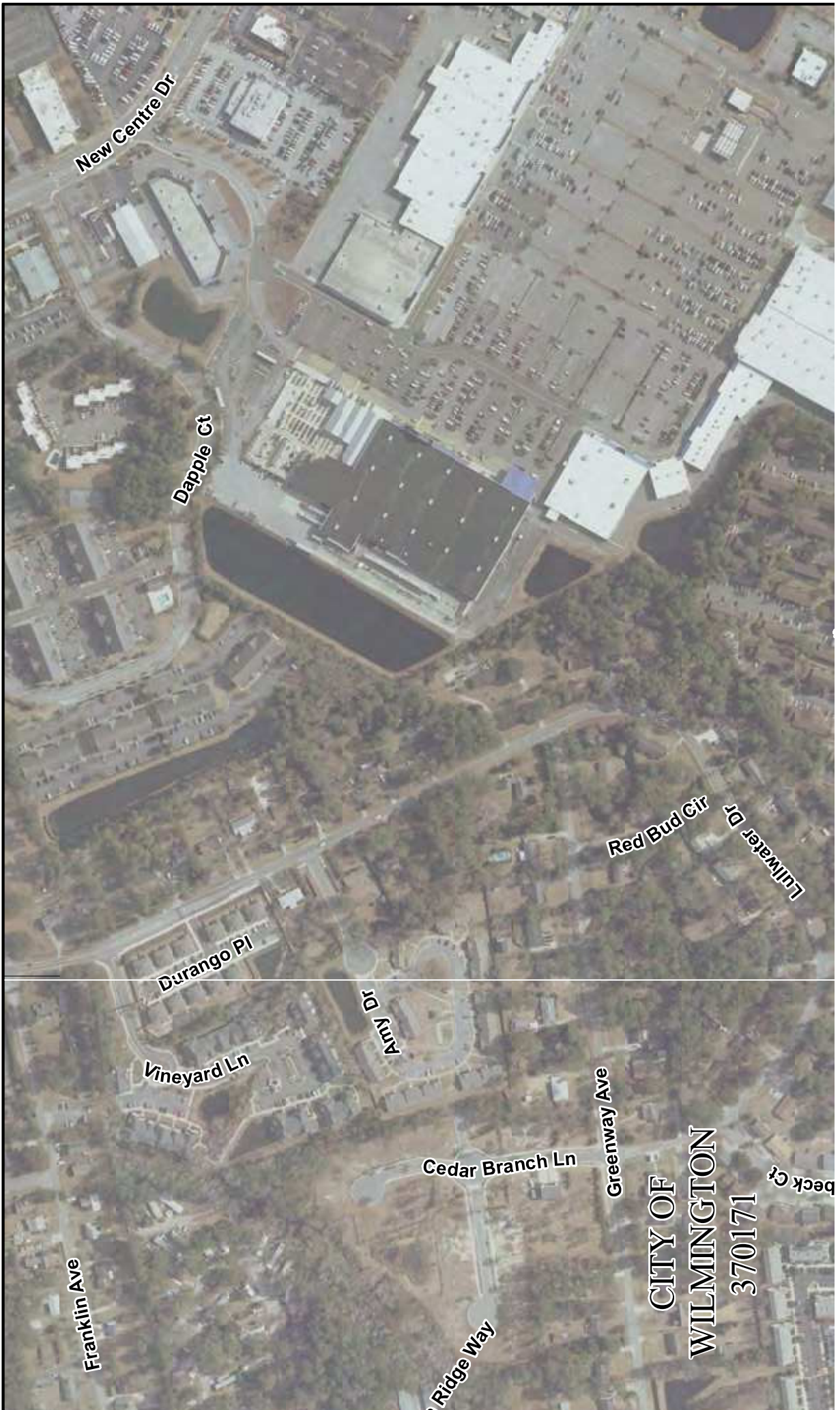
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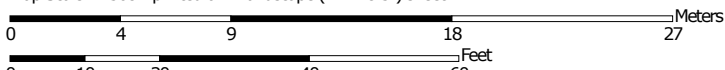


CITY OF
WILMINGTON
370171

Soil Map—New Hanover County, North Carolina




Map Scale: 1:308 if printed on A landscape (11" x 8.5") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: New Hanover County, North Carolina
 Survey Area Data: Version 16, Sep 29, 2015

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

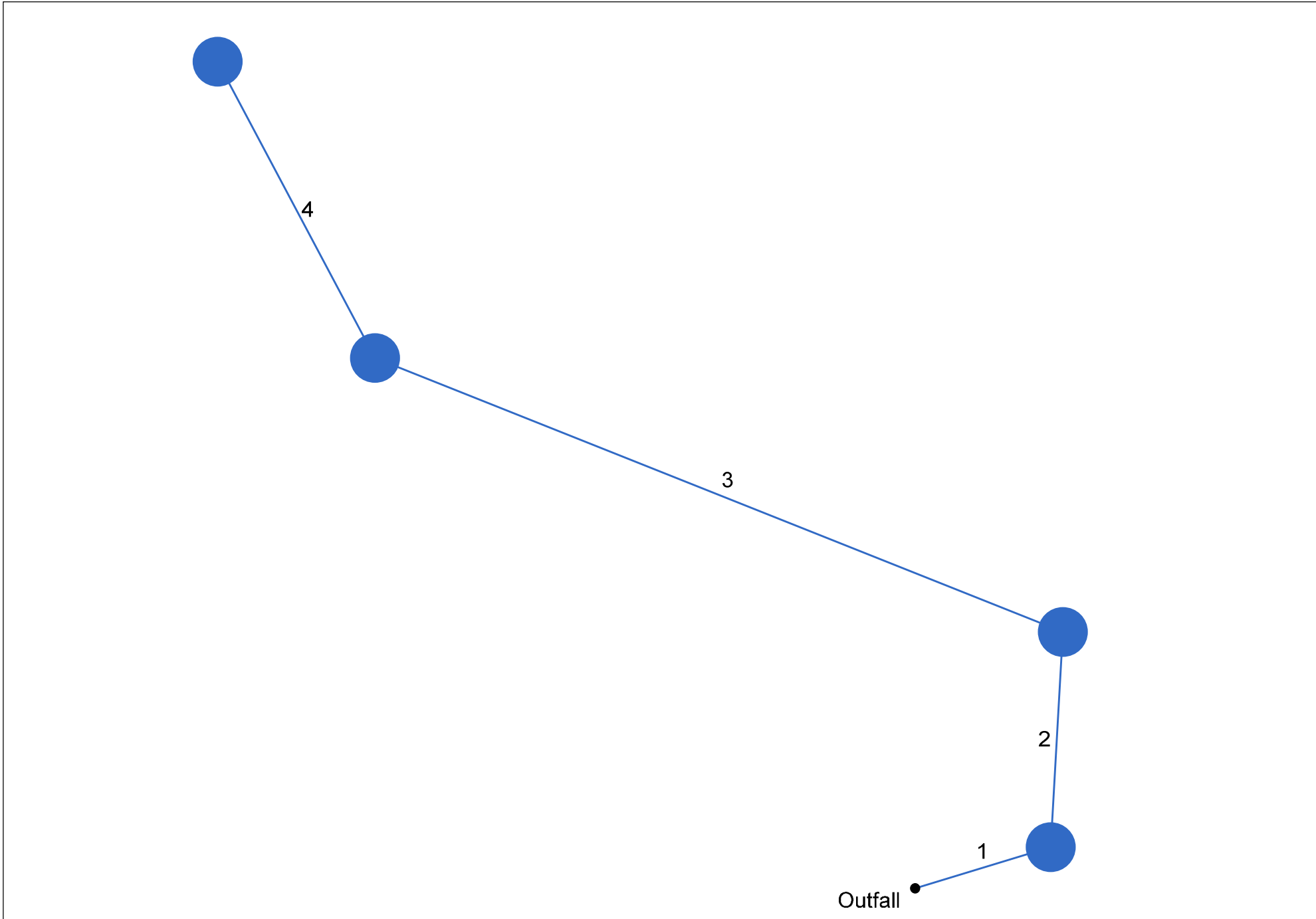
Date(s) aerial images were photographed: Data not available.

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

New Hanover County, North Carolina (NC129)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Le	Leon sand	0.3	100.0%
Totals for Area of Interest		0.3	100.0%

Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



Project File: Pipe Network.stm

Number of lines: 4

Date: 11/4/2016

Storm Sewer Inventory Report

Line No.	Alignment				Flow Data				Physical Data								Line ID
	Dnstr Line No.	Line Length (ft)	Defl angle (deg)	Junc Type	Known Q (cfs)	Drng Area (ac)	Runoff Coeff (C)	Inlet Time (min)	Invert El Dn (ft)	Line Slope (%)	Invert El Up (ft)	Line Size (in)	Line Shape	N Value (n)	J-Loss Coeff (K)	Inlet/ Rim El (ft)	
1	End	12.060	-20.647	DrCrb	0.00	0.56	0.60	5.0	37.49	0.33	37.53	15	Cir	0.012	1.40	39.60	
2	1	22.210	-66.721	DrCrb	0.00	0.22	0.75	5.0	37.53	0.50	37.64	15	Cir	0.012	1.40	39.60	
3	2	63.880	-66.387	DrCrb	0.00	0.03	0.50	5.0	37.64	0.50	37.96	15	Cir	0.012	1.05	40.50	
4	3	33.250	40.554	DrCrb	0.00	0.09	0.70	5.0	37.96	0.51	38.13	15	Cir	0.012	1.00	40.60	
Project File: Pipe Network.stm												Number of lines: 4				Date: 11/4/2016	

Structure Report

Struct No.	Structure ID	Junction Type	Rim Elev (ft)	Structure			Line Out			Line In		
				Shape	Length (ft)	Width (ft)	Size (in)	Shape	Invert (ft)	Size (in)	Shape	Invert (ft)
1		DropCurb	39.60	Cir	4.00	4.00	15	Cir	37.53	15	Cir	37.53
2		DropCurb	39.60	Cir	4.00	4.00	15	Cir	37.64	15	Cir	37.64
3		DropCurb	40.50	Cir	4.00	4.00	15	Cir	37.96	15	Cir	37.96
4		DropCurb	40.60	Cir	4.00	4.00	15	Cir	38.13			

Project File: Pipe Network.stm

Number of Structures: 4

Run Date: 11/4/2016

Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	
1	End	12.060	0.56	0.90	0.60	0.34	0.58	5.0	8.1	8.5	4.93	4.03	4.02	15	0.33	37.49	37.53	38.74	38.78	39.84	39.60	
2	1	22.210	0.22	0.34	0.75	0.17	0.24	5.0	7.9	8.6	2.09	4.92	1.70	15	0.50	37.53	37.64	39.13	39.15	39.60	39.60	
3	2	63.880	0.03	0.12	0.50	0.02	0.08	5.0	6.1	9.3	0.72	4.95	0.59	15	0.50	37.64	37.96	39.21	39.22	39.60	40.50	
4	3	33.250	0.09	0.09	0.70	0.06	0.06	5.0	5.0	9.7	0.61	5.00	0.52	15	0.51	37.96	38.13	39.23	39.23	40.50	40.60	

Project File: Pipe Network.stm

Number of lines: 4

Run Date: 11/4/2016

NOTES: Intensity = $96.48 / (\text{Inlet time} + 12.40)^{0.80}$; Return period = Yrs. 10 ; c = cir e = ellip b = box

Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream								Len (ft)	Upstream								Check		JL coeff (K)	Minor loss (ft)
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy loss (ft)		
1	15	4.93	37.49	38.74	1.25	1.23	4.02	0.25	38.99	0.497	12.060	37.53	38.78	1.25	1.23	4.02	0.25	39.03	0.493	0.495	0.060	1.40	0.35
2	15	2.09	37.53	39.13	1.25	1.23	1.70	0.05	39.18	0.089	22.210	37.64	39.15	1.25	1.23	1.70	0.04	39.20	0.089	0.089	0.020	1.40	0.06
3	15	0.72	37.64	39.21	1.25	1.23	0.59	0.01	39.22	0.011	63.880	37.96	39.22	1.25	1.23	0.59	0.01	39.23	0.011	0.011	0.007	1.05	0.01
4	15	0.61	37.96	39.23	1.25	1.23	0.50	0.00	39.23	0.008	33.250	38.13	39.23	1.10	1.14	0.54	0.00	39.23	0.007	0.007	0.002	1.00	0.00

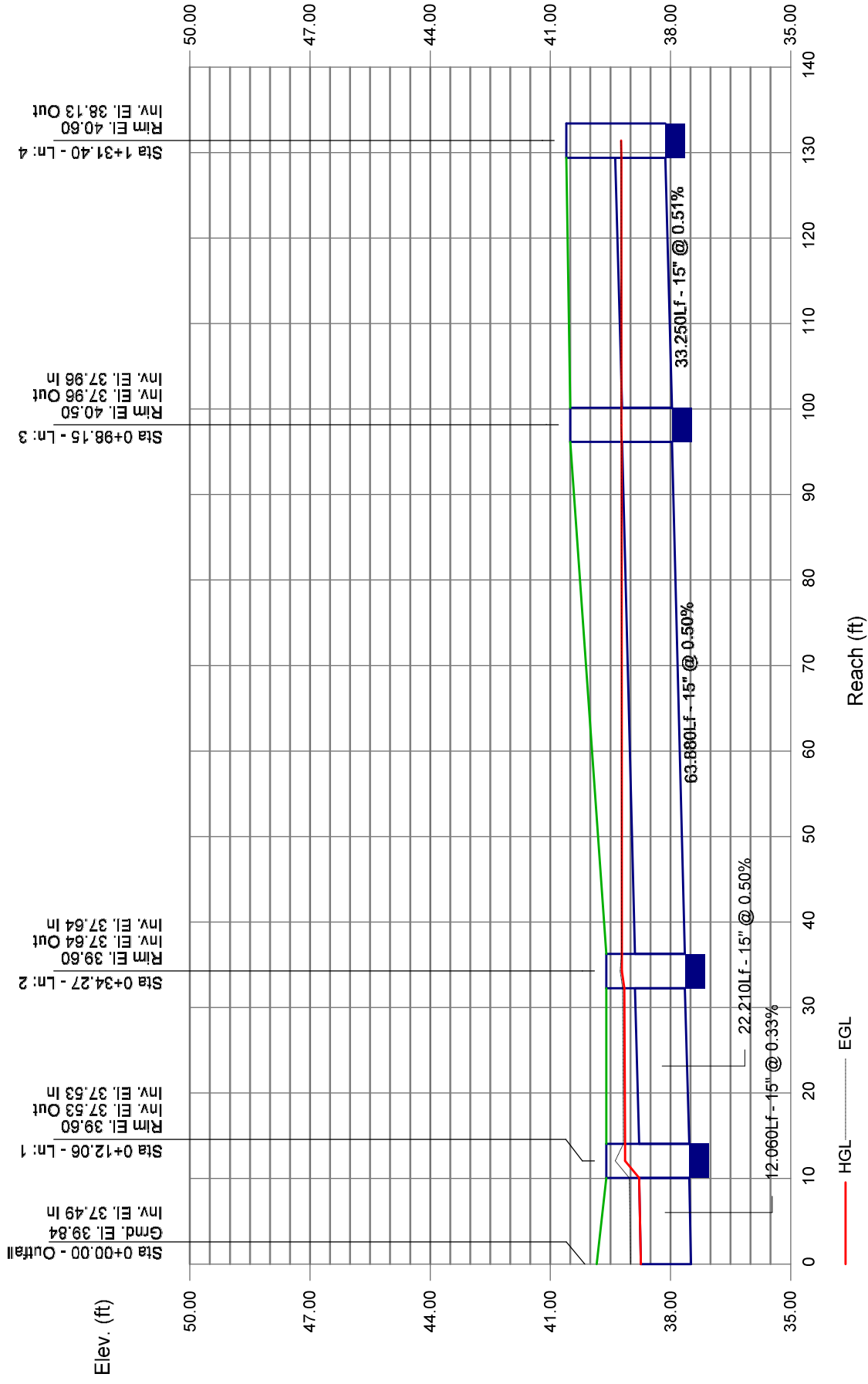
Project File: Pipe Network.stm

Number of lines: 4

Run Date: 11/4/2016

; c = cir e = ellip b = box

Storm Sewer Profile



Storm Sewer Tabulation

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	
1	End	12.060	0.56	0.90	0.60	0.34	0.58	5.0	7.5	10.7	6.18	4.03	5.03	15	0.33	37.49	37.53	38.74	38.83	39.84	39.60	
2	1	22.210	0.22	0.34	0.75	0.17	0.24	5.0	7.4	10.7	2.61	4.92	2.13	15	0.50	37.53	37.64	39.39	39.42	39.60	39.60	
3	2	63.880	0.03	0.12	0.50	0.02	0.08	5.0	5.9	11.4	0.89	4.95	0.73	15	0.50	37.64	37.96	39.51	39.53	39.60	40.50	
4	3	33.250	0.09	0.09	0.70	0.06	0.06	5.0	5.0	11.9	0.75	5.00	0.61	15	0.51	37.96	38.13	39.53	39.54	40.50	40.60	

Project File: Pipe Network.stm

Number of lines: 4

Run Date: 11/4/2016

NOTES: Intensity = $78.44 / (\text{Inlet time} + 10.10)^{0.70}$; Return period = Yrs. 50 ; c = cir e = ellip b = box

Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream								Len (ft)	Upstream								Check		JL coeff (K)	Minor loss (ft)
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy loss (ft)		
1	15	6.18	37.49	38.74	1.25	1.23	5.03	0.39	39.13	0.780	12.060	37.53	38.83	1.25	1.23	5.03	0.39	39.23	0.780	0.780	0.094	1.40	0.55
2	15	2.61	37.53	39.39	1.25	1.23	2.13	0.07	39.46	0.139	22.210	37.64	39.42	1.25	1.23	2.13	0.07	39.49	0.139	0.139	0.031	1.40	0.10
3	15	0.89	37.64	39.51	1.25	1.23	0.73	0.01	39.52	0.016	63.880	37.96	39.53	1.25	1.23	0.73	0.01	39.53	0.016	0.016	0.010	1.05	0.01
4	15	0.75	37.96	39.53	1.25	1.23	0.61	0.01	39.54	0.011	33.250	38.13	39.54	1.25	1.23	0.61	0.01	39.54	0.011	0.011	0.004	1.00	0.01

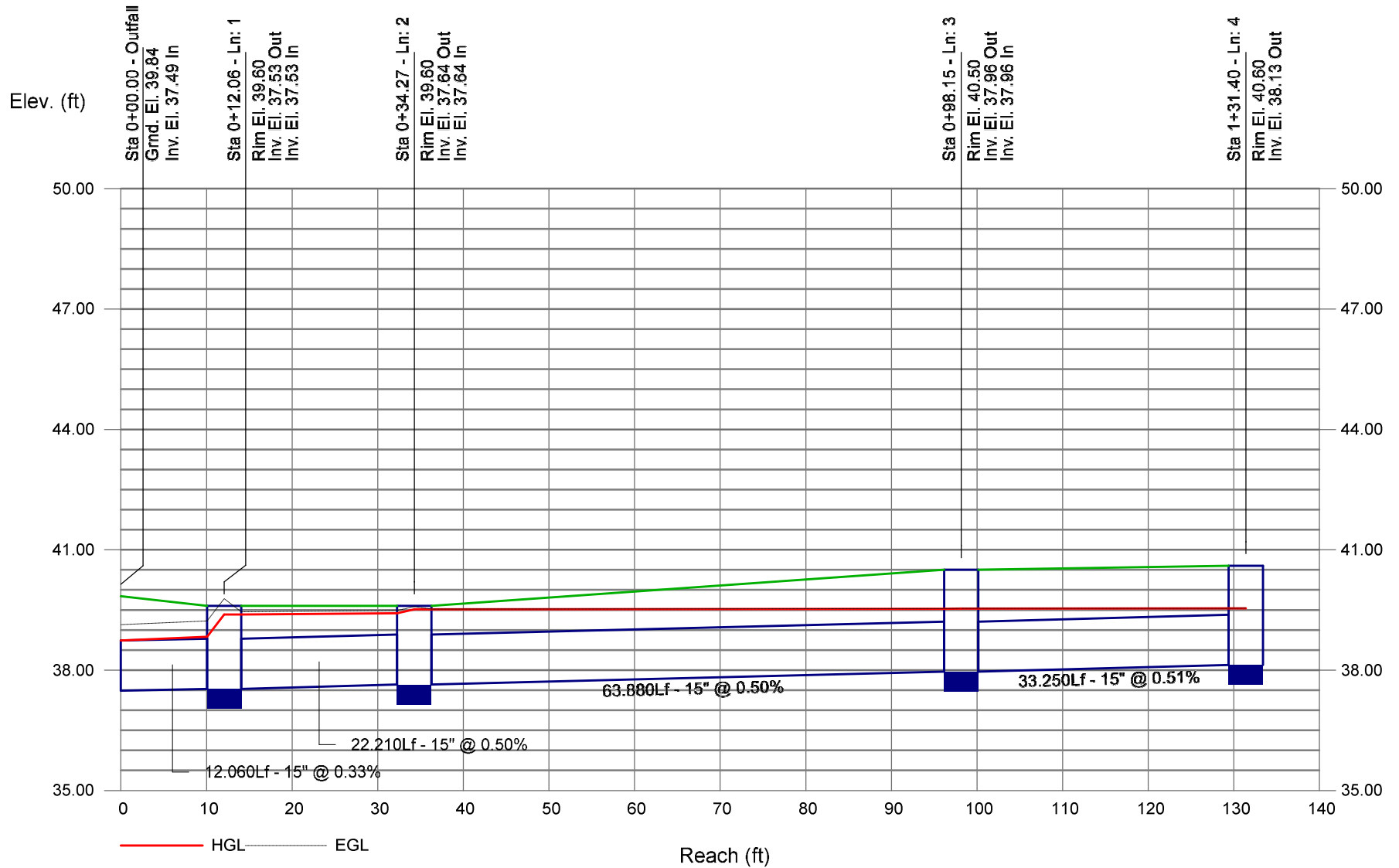
Project File: Pipe Network.stm

Number of lines: 4

Run Date: 11/4/2016

; c = cir e = ellip b = box

Storm Sewer Profile



Wet Detention Basin Modification Calculations

Project: Hawthorne at New Centre
 Location: Wilmington, NC
 Date: 5/24/2016

Pond Number: 1

Total Project Area: sf or ac

Total On-Site Drainage Area: sf or ac

Off-site Drainage Area: sf or ac

Total: ac.

On-Site Impervious Area:

Buildings (Existing):	<input type="text" value="101,295"/>	sf
Parking & Roads (Existing):	<input type="text" value="263,236"/>	sf
Sidewalks (Existing):	<input type="text" value="42,032"/>	sf
New Impervious:	<input type="text" value="4,990"/>	sf
Future Impv. (from Mod):	<input type="text" value="5,000"/>	sf
Off-Site Impervious:	<input type="text" value="0"/>	sf

Originally Approved Imp. Area:

Original Approved % Imp:

Modified Watershed % Imp:

(including new Imp. Area)

Total New Impervious Area:

Total Impervious Area: sf or ac.

Calculate Required Surface Area:

Avg. Perm. Pool Depth: 7 Feet (per permit)

SA/DA Ratio: 2.08

Minimum Required Surface Area: sf

Calculate Original WQv Storage Volume:

Use Simple Method with volume for 1.0" storm (per original pond design):

$R_v = 0.05 + 0.009(I)$

R_v = Runoff Coefficient (ratio of runoff to rainfall in inches)

I_o = Impervious Percentage-Original

$R_v =$

$WQ_v = 3630 \times R_d \times R_v \times A$

R_d = Design Storm = 1.0"

A = Drainage Area

$WQ_v =$ cf

WQ_v = Storage Volume

Calculate Delta WQv Storage Volume (based on new impervious area only):

Use Simple Method with volume for 1.5" storm (for new impervious area):

$R_v = 0.05 + 0.009(I)$

$R_v =$ Runoff Coefficient (ratio of runoff to rainfall in inches)

$I_p =$ Impervious Percentage-Additional= 100%

(Assume additional impervious area is separate watershed with 100% imp. coverage)

$R_v =$

$WQ_v = 3630 \times R_d \times R_v \times A$

$R_d =$ Design Storm= 1.5"

$A =$ Drainage Area-New Impervious Area Only

$WQ_v =$ cf

$WQ_v =$ Storage Volume

Total $WQ_v =$ Original WQ_v Volume + Delta WQ_v Volume

Total $WQ_v =$ cf

Elevation	Contour Area	Inc. Volume	Accumulated Volume	Stage
	(sf)	(cf)	(cf)	
35.10	27500	0	0	0
35.50	28301	11160	11160	0.4
36.00	29320	14405	25565	0.9
36.50	30356	14919	40484	1.4
37.00	31410	15442	55926	1.9

Calculated S-S Parameters:

$b =$
 $K_s =$

Orifice El: 35.10

Overflow El: 37.00

Overflow Spillway Stage: ft
 Spillway Crest Length: ft
 Storage Below Overflow: cf

$S = K_s \times Z^b$

WQv Stage: or Elevation
Surface Area at WQv Stage: Square Feet

Calculate WQv Drawdown Time:

Drawdown Orifice Diameter: Cross Section Area: sf
 Orifice Coefficient: Average Head: ft
 Number of Orifices: Discharge: cfs

WQv Drawdown Time: hours or days

Weighted Curve Number Calculation

Existing Impervious Percentage:

52.4643%

New Impervious Percentage:

53.7535%

Hydraulic Soil Group:

Leon, Murville

Use HSG C

Curve Numbers:

Impervious: 98

Grass, Good Condition: 74

Existing Weighted CN: 86.59

New Weighted CN: 86.90

Based on the Weighted Curve number, pond flood routing and overflow hydraulics should remain the same. Note that this analysis does not constitute a flood-routing analysis of the existing pond.



NOAA Atlas 14, Volume 2, Version 3
Location name: Wilmington, North Carolina, US*
Latitude: 34.2387°, Longitude: -77.8797°
Elevation: 41 ft*
 * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF_tabular](#) | [PF_graphical](#) | [Maps & aerals](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	6.28 (5.87-6.76)	7.45 (6.95-8.02)	8.72 (8.14-9.36)	9.72 (9.02-10.4)	11.0 (10.2-11.8)	11.9 (11.0-12.8)	12.9 (11.8-13.8)	13.9 (12.6-14.9)	15.1 (13.6-16.3)	16.1 (14.4-17.4)
10-min	5.01 (4.69-5.39)	5.96 (5.56-6.41)	6.98 (6.51-7.50)	7.78 (7.22-8.35)	8.75 (8.09-9.37)	9.49 (8.74-10.2)	10.2 (9.38-11.0)	11.0 (9.99-11.8)	12.0 (10.8-12.9)	12.7 (11.3-13.7)
15-min	4.18 (3.90-4.50)	5.00 (4.66-5.37)	5.89 (5.49-6.32)	6.56 (6.09-7.04)	7.39 (6.84-7.92)	8.01 (7.38-8.60)	8.64 (7.91-9.26)	9.24 (8.40-9.92)	10.0 (9.03-10.8)	10.6 (9.49-11.5)
30-min	2.86 (2.68-3.08)	3.45 (3.22-3.71)	4.19 (3.90-4.49)	4.75 (4.41-5.10)	5.47 (5.06-5.86)	6.03 (5.55-6.47)	6.61 (6.05-7.09)	7.19 (6.54-7.72)	7.98 (7.19-8.60)	8.61 (7.68-9.28)
60-min	1.78 (1.67-1.92)	2.16 (2.02-2.33)	2.68 (2.50-2.88)	3.09 (2.87-3.32)	3.65 (3.37-3.90)	4.09 (3.76-4.38)	4.55 (4.17-4.88)	5.04 (4.59-5.42)	5.72 (5.16-6.17)	6.29 (5.61-6.78)
2-hr	1.05 (0.972-1.15)	1.28 (1.18-1.40)	1.64 (1.51-1.78)	1.93 (1.77-2.11)	2.36 (2.16-2.57)	2.73 (2.48-2.97)	3.13 (2.83-3.40)	3.57 (3.20-3.87)	4.22 (3.75-4.59)	4.78 (4.21-5.22)
3-hr	0.750 (0.693-0.821)	0.911 (0.840-0.996)	1.17 (1.07-1.27)	1.39 (1.27-1.51)	1.72 (1.57-1.87)	2.01 (1.82-2.19)	2.33 (2.10-2.53)	2.69 (2.40-2.92)	3.24 (2.85-3.51)	3.72 (3.23-4.04)
6-hr	0.467 (0.432-0.512)	0.568 (0.525-0.622)	0.728 (0.671-0.797)	0.868 (0.797-0.948)	1.08 (0.983-1.17)	1.26 (1.15-1.37)	1.47 (1.32-1.60)	1.70 (1.52-1.85)	2.06 (1.81-2.24)	2.37 (2.06-2.58)
12-hr	0.272 (0.249-0.300)	0.330 (0.302-0.363)	0.426 (0.390-0.469)	0.511 (0.465-0.560)	0.639 (0.577-0.699)	0.753 (0.676-0.822)	0.882 (0.787-0.963)	1.03 (0.907-1.12)	1.26 (1.09-1.37)	1.46 (1.25-1.59)
24-hr	0.161 (0.147-0.179)	0.195 (0.178-0.218)	0.253 (0.230-0.281)	0.303 (0.275-0.337)	0.381 (0.342-0.422)	0.451 (0.401-0.499)	0.530 (0.466-0.587)	0.620 (0.538-0.688)	0.759 (0.645-0.848)	0.883 (0.737-0.991)
2-day	0.095 (0.087-0.106)	0.115 (0.106-0.128)	0.148 (0.135-0.164)	0.176 (0.161-0.195)	0.220 (0.198-0.243)	0.258 (0.230-0.286)	0.301 (0.266-0.335)	0.350 (0.304-0.391)	0.425 (0.361-0.477)	0.490 (0.410-0.554)
3-day	0.068 (0.062-0.075)	0.082 (0.075-0.090)	0.104 (0.095-0.115)	0.124 (0.113-0.137)	0.153 (0.138-0.169)	0.179 (0.160-0.198)	0.207 (0.183-0.230)	0.239 (0.209-0.267)	0.288 (0.246-0.323)	0.331 (0.278-0.374)
4-day	0.054 (0.050-0.060)	0.065 (0.060-0.072)	0.082 (0.075-0.091)	0.097 (0.089-0.107)	0.120 (0.108-0.132)	0.139 (0.124-0.153)	0.160 (0.142-0.178)	0.184 (0.161-0.205)	0.219 (0.189-0.246)	0.251 (0.212-0.283)
7-day	0.035 (0.033-0.039)	0.043 (0.040-0.047)	0.054 (0.050-0.059)	0.063 (0.058-0.069)	0.076 (0.070-0.083)	0.088 (0.080-0.096)	0.100 (0.090-0.110)	0.114 (0.101-0.125)	0.134 (0.117-0.148)	0.150 (0.130-0.167)
10-day	0.028 (0.026-0.030)	0.034 (0.031-0.036)	0.042 (0.039-0.045)	0.048 (0.045-0.053)	0.058 (0.053-0.063)	0.066 (0.061-0.072)	0.075 (0.068-0.082)	0.085 (0.076-0.093)	0.099 (0.087-0.109)	0.110 (0.096-0.123)
20-day	0.019 (0.018-0.020)	0.022 (0.021-0.024)	0.027 (0.025-0.029)	0.031 (0.029-0.034)	0.037 (0.034-0.040)	0.042 (0.038-0.045)	0.047 (0.043-0.051)	0.052 (0.047-0.057)	0.060 (0.053-0.065)	0.066 (0.058-0.073)
30-day	0.015 (0.014-0.016)	0.018 (0.017-0.019)	0.022 (0.021-0.023)	0.025 (0.023-0.026)	0.029 (0.027-0.031)	0.032 (0.030-0.034)	0.036 (0.033-0.038)	0.039 (0.036-0.042)	0.044 (0.040-0.048)	0.048 (0.043-0.052)
45-day	0.013 (0.012-0.014)	0.015 (0.014-0.016)	0.018 (0.017-0.019)	0.020 (0.019-0.021)	0.023 (0.022-0.025)	0.026 (0.024-0.027)	0.028 (0.026-0.030)	0.031 (0.029-0.033)	0.035 (0.032-0.037)	0.037 (0.034-0.041)
60-day	0.012 (0.011-0.012)	0.014 (0.013-0.014)	0.016 (0.015-0.017)	0.018 (0.017-0.019)	0.020 (0.019-0.021)	0.022 (0.021-0.023)	0.024 (0.022-0.026)	0.026 (0.024-0.028)	0.028 (0.026-0.031)	0.030 (0.028-0.033)

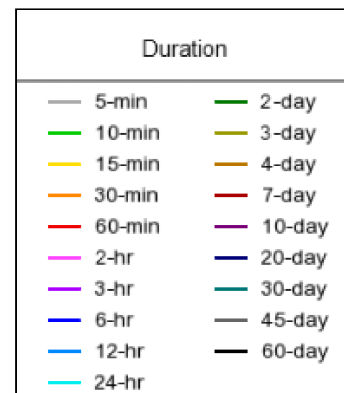
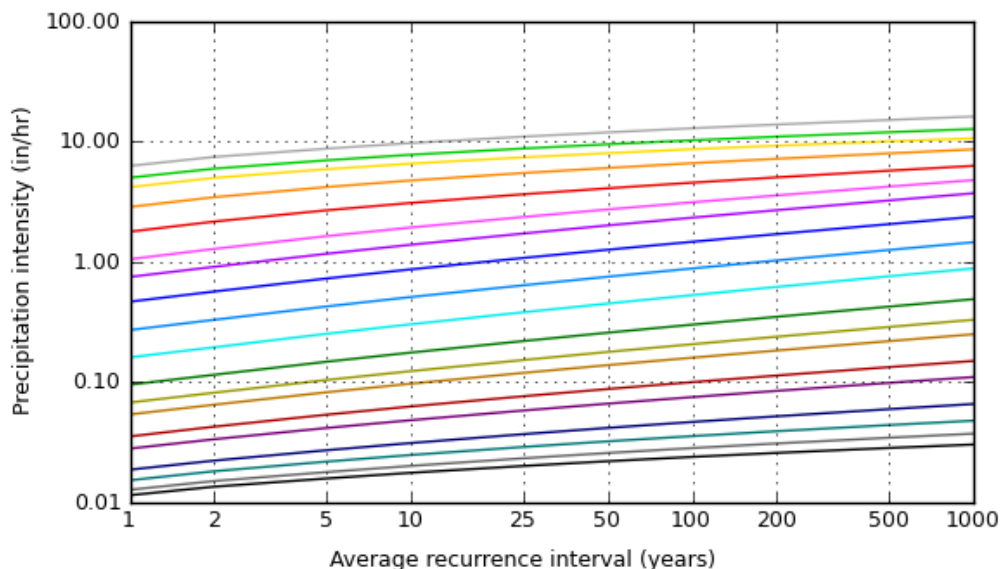
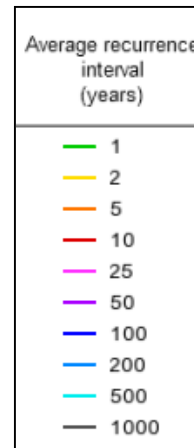
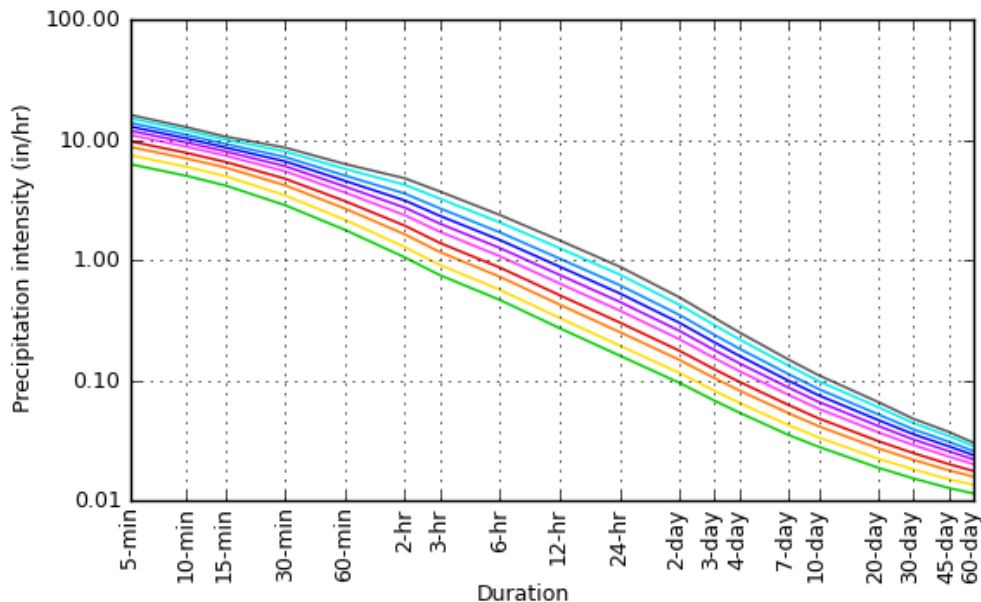
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)

PF graphical

PDS-based intensity-duration-frequency (IDF) curves

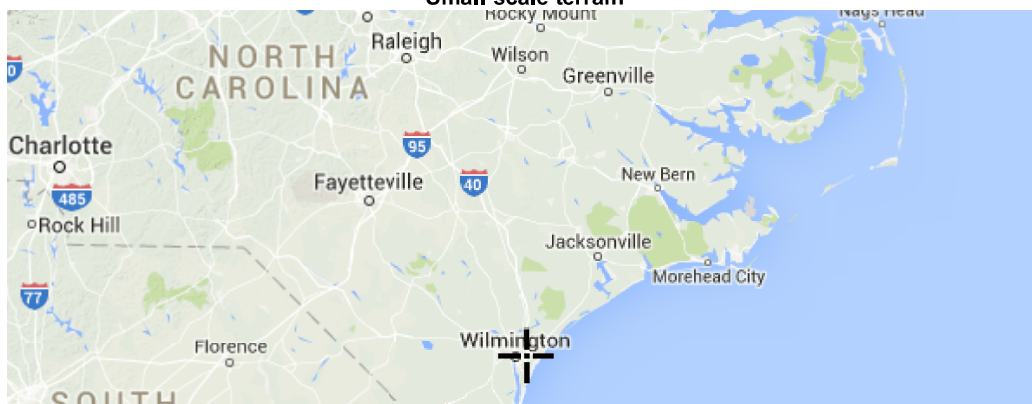
Latitude: 34.2387°, Longitude: -77.8797°



[Back to Top](#)

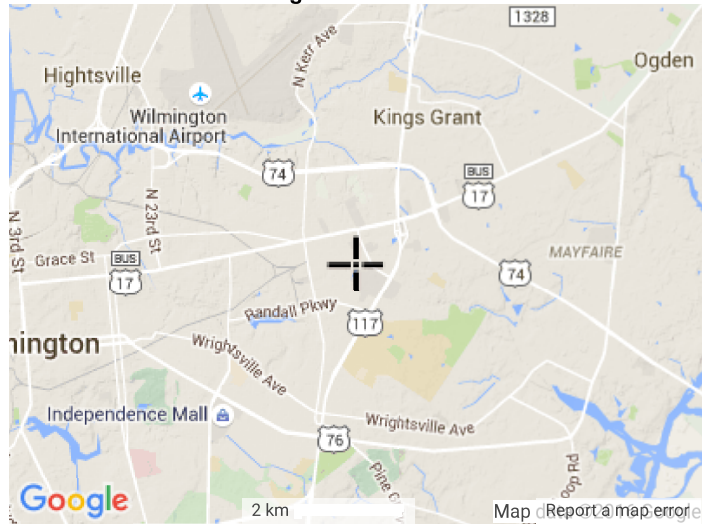
Maps & aerials

Small scale terrain

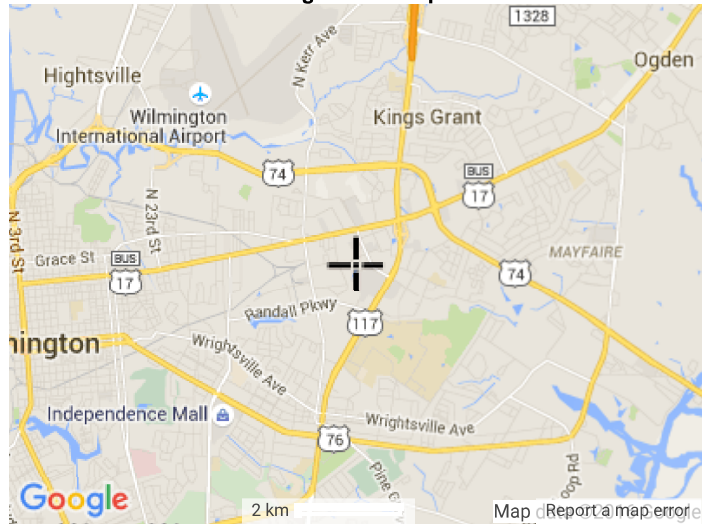




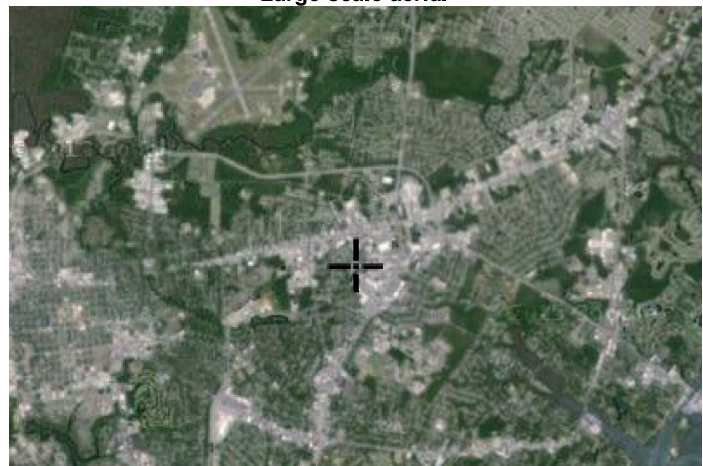
Large scale terrain



Large scale map



Large scale aerial





[Back to Top](#)

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1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

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